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Development of Low Energy X-ray Detectors using LGAD Sensors

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Abstract

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Recent advances in segmented Low Gain Avalanche Detectors (LGADs) make them interesting for the detection of low energy X-rays photons thanks to their internal gain. LGAD microstrip sensors fabricated by Fondazione Bruno Kessler have been investigated using X-rays with both charge-integrating and single photon-counting readout chips developed at the Paul Scherrer Institut. The charge multiplication occurring in the sensor allows the detection of X-rays with improved Signal-to-Noise Ratio without additional dark counts. The application in the tender X-ray energy range is demonstrated by the detection of the sulphur K_{α} and K_{β} lines (2.3 and 2.46 keV) in an energy dispersive fluorescence spectrometer at the Swiss Light Source. Although improvements in the segmentation and in the quantum efficiency at low energy are still necessary, this work paves the way for the development of single photon-counting detectors in the soft X-ray energy range.

1. Introduction

1.1. Motivation

The advent of large area single photon-counting hybrid detectors developed at the Swiss Light Source allowed huge improvements in many hard X-ray imaging techniques e.g. macromolecular crystallography (Henrich, 2009), powder diffraction (Bergamaschi, 2010) and microscopy (Guizar-Sicarios, 2014). More recently, the development of charge-integrating detectors with single photon resolution and large dynamic range promises to extend the range of application of hybrid detectors to XFEL experiments and to improve the performance in high flux synchrotron experiments (Henrich, 2011; Mozzanica, 2016). Nevertheless, many synchrotron experiments are performed in the soft X-ray energy range (Hitchcock, 2015) due to the higher cross section for thin or low interacting samples and to the presence of the K-edges of many light elements useful e.g. in macromolecular crystallography (Liebschner, 2016) and L-edges

14 of 3D transition metals which are relevant to study copper based superconductors or
15 magnetic structures by means of Scanning X-ray Transmission Microscopy (STXM),
16 ptychography or resonant diffraction (Fink, 2013). These applications are often hin-
17 dered by the detector performance and usually rely on photodiodes (Gullikson, 1996)
18 and CCDs (Müller et al., 2016). Photodiodes provide a large dynamic range, but they
19 have a relatively high noise which results in low sensitivity and they are not position
20 sensitive. This results in long scanning procedures for alignment and loss of possibly
21 interesting information e.g. in STXM experiments. On the other hand, CCDs provide
22 very low noise (Strüder, 2010; Hall et al., 2011) and high spatial resolution, but they
23 can only run at limited frame rates due to the relatively slow readout times, require
24 a fast shutter and deep cooling, have limited dynamic range due to the full-well-
25 capacity and can easily suffer from radiation damage. Lately many developments have
26 tried to overcome these limitations (Denes, 2011). Recently, Complementary Metal-
27 Oxide-Semiconductor (CMOS) monolithic detectors are also being commissioned for
28 soft X-ray applications (Wunderer, 2014). However, these monolithic detectors still
29 have to prove their performance in terms of versatility, robustness and reliability at
30 the level that hybrid detectors provide at higher energies.

31 Position sensitive hybrid detectors, as opposite to monolithic, are composed of two
32 separate parts: a sensor where the X-rays convert into electric charge and the readout
33 electronics where the signal is processed and eventually stored or digitized. The sensor
34 is a semiconductor material, normally silicon, where X-rays convert to electron-hole
35 pairs with an electron-hole (e^-h) pair generation energy of 3.6 eV, segmented into
36 strips (1D) or pixels (2D) in order to provide position sensitivity. Each single element is
37 connected independently to its readout channel of the electronics for highly parallelized
38 performance. This interconnection is obtained by means of wire-bonding (for strips)
39 or bump-bonding (for pixels), introducing a non-negligible capacitance at the input of

40 the readout electronics with a consequent increased noise. For this reason, hybrid strip
 41 and pixel detectors have traditionally not been used for soft X-rays, which produce a
 42 low signal comparable to the noise of the readout electronics.

43 The noise of a detector is usually defined by the Equivalent Noise Charge (*ENC*)
 44 (Radeka, 1988) i.e. the charge at the detector input needed to create the same noise
 45 at the output. This affects the energy resolution and the presence of noise in the
 46 final image, and can be converted from electrons into energy by applying the $e^{-}h$
 47 pair generation energy of the semiconductor material used. In Photon Counting (PC)
 48 detectors, a threshold E_t is applied to the comparator integrated in the frontend
 49 electronics and a photon is counted only if the signal generated by a photon exceeds
 50 it. In case of monochromatic radiation, E_t is normally set to half of the X-ray energy in
 51 order to optimize the quantum efficiency of the detector while avoiding multiple counts
 52 due to charge sharing (Kraft, 2009). Equivalently, E_t can be applied offline to the
 53 analog data readout from Charge Integrating (CI) detectors in order to discriminate
 54 the signal from the noise.

55 The number of noise counts N_n for the same threshold E_t in a given measurement
 56 time T depends on the *ENC* of the detector, but is different for PC and CI detector
 57 with the same noise. In the case of a PC detector, N_n depends on both the *ENC* and
 58 the bandwidth of the noise. It can be estimated by considering the rate of positive
 59 zero crossings f_n (Bendat, 1958), resulting in:

$$N^{PC} = \frac{T \cdot f_n}{2\pi} e^{\frac{-E_t^2}{2\sigma_{ENC}^2}} \quad (1)$$

60 where f_n depends on the shaping parameters of the frontend electronics and is usually
 61 in the range 1–20 MHz. Considering a relatively slow detector with $f_n=2$ MHz, one
 62 would need a threshold higher than $5\sigma_{ENC}$ to have less than 0.1 % noise counts per
 63 second (which sums to 1 kcounts in a 1 Mpixel detector). Even with an noise as low as

⁶⁴ $\sigma_{ENC}=46 e^-$ as described in Wicek (2015), one obtains a minimum detectable energy

65 higher than $550 e^- \cdot 3.6 \text{ eV}/e^- \approx 2 \text{ keV}$. By setting the threshold higher than half of
 66 the X-ray energy, PC detectors can be used below this energy slightly compromising
 67 the quantum efficiency, as described in Donath (2013) down to 1.75 keV.

68

69 On the other hand, in a CI detector, the noise is sampled at the readout and can

70 increase with the exposure time Δt , due to the leakage current of the

71 to the bandwidth of the frontend electronics. However, for CI hybrid

72 normally necessary to subdivide long measurement times $T > 1-10$

73 frames $n_f = T/\Delta t$ with short exposure time Δt . Therefore the number

74 N_n during the exposure time T for a CI detector is (Becker, 2012):

$$N_n^{CI} = \frac{T}{\Delta t} \frac{1 - \text{Erf}\left(\frac{\sqrt{E_t}}{2\sigma_{ENC}}\right)}{2} \quad (2)$$

75 Considering an acceptable exposure time $\Delta t \sim 1 \text{ ms}$ without challenging cooling

76 requirements, a threshold cut at $5\sigma_{ENC}$ is required to have less than 0.1 % noise counts

77 per second (which sums to 1 kcounts in a 1 Mpixel detector). Low noise CI detectors

78 have been developed with an $ENC \sim 30 e^-$ (Jungmann-Smith, 2016; Cartier, 2016),

79 resulting in single photon resolution at a minimum energy of $300 e^- \cdot 3.6 \text{ eV}/e^- = 1.08 \text{ keV}$.

80 This scales of a factor of 2 in case of small pixels in order to allow charge summation

81 to suppress charge sharing (Cartier, 2016).

82 However, while the minimum value of $E_t = 5\sigma_{ENC}$ defines a corresponding mini-

83 mum energy that can be detected by PC detectors, CI detectors can also be operated

84 a low energies without single photon resolution. Being f_n about three orders of mag-

85 nitude higher than $1/\Delta t$, the number of noise counts at the same threshold and noise

86 is much higher for a PC than for a CI detector.

87 The ENC of state-of-the-art readout electronics needs to be reduced

88 order of magnitude in order to make soft X-ray energies energies, spanning from the

89 iron L-edge at 708 eV for magnetic studies down to the carbon K-edge at 250 eV for 8

90 imaging of biological specimen, accessible to single photon counting detectors. For this
91 reason, an amplification of the signal in the sensor as the one provided by Low Gain
92 Avalanche Detectors (LGAD) would help to reduce the minimum detectable energy.
93 Moreover, the outstanding timing performance of LGAD sensors, originally developed
94 for tracking charged particles with ~ 10 -20 picosecond timing resolution, could also
95 find applications for time resolved soft X-ray applications (Puzic et al., 2010).

96 *1.2. Low Gain Avalanche Detectors*

97 The development of LGAD sensors is based on the concept of the standard Avalanche
98 Photo Diodes (APD) (Lutz, 2007; Tapan, 1997; Pellegrini, 2014; Pellegrini, 2016). The
99 APDs offer a gain from a few tens to hundreds and they can be used for single photon
100 detection in the visible down to the infrared energy range. However, with such a high
101 gain, the noise performance is degraded due to the significant increase of shot-noise
102 caused by the amplified signal as well as by the leakage current, and thus worsen the
103 signal-to-noise ratio. APDs are fabricated only in small arrays with a pitch of hun-
104 dreds of microns (Johnson, 2009) and provide an extremely high time resolution. In
105 the hard X-ray energy range they usually exploit indirect conversion in a scintillator
106 since full depletion requires very high voltages (~ 1000 V) due to the presence of a
107 highly doped region below the junction.

108 More recently, Silicon Photo Multipliers (SiPMs) have greatly advanced the tech-
109 nology for the fabrication of segmented amplifying devices, with channel densities that
110 can be up to 10^4 mm^{-2} . While an APD is usually operated using a bias voltage such
111 that the amplified signal stays proportional to the detected one, SiPM are specifically
112 designed to operate with a reverse bias voltage well above the breakdown voltage i.e. in
113 Geiger mode. The resulting gain is of the order of 10^6 , but with the disadvantage of a
114 high dark count density even in absence of illumination ($10^5 - 10^6$ pulses/s/ mm^2) and

115 a non-negligible probability of afterpulsing i.e. detection of a spurious

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116 single photon arrival (Bhuzan et al., 2003).

probability

117 The LGAD sensors are built-up on a similar technology as APDs and SiPMs but
118 implemented with a lower concentration of dopants at the junction to reduce the

and SiPMs but
to reduce the

119 gain to 5–20. LGADs amplify the signal induced by charged particles or photons,
120 generate an output signal which is proportional to the deposited energy and result in
121 an improvement on the signal-to-noise ratio.

122 Charge multiplication, also known as impact ionization, is the most important mech-
123 anism during the operation of LGAD sensors. At the $p-n$ junction, due to the presence
124 of additional dopants (typically with a peak concentration of $\sim 10^{16} - 10^{17} \text{ cm}^{-3}$),
125 which is significantly higher than the doping concentration of the silicon substrate
126 ($\sim 10^{11} - 10^{12} \text{ cm}^{-3}$), a high electric field is built-up

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at the junction,

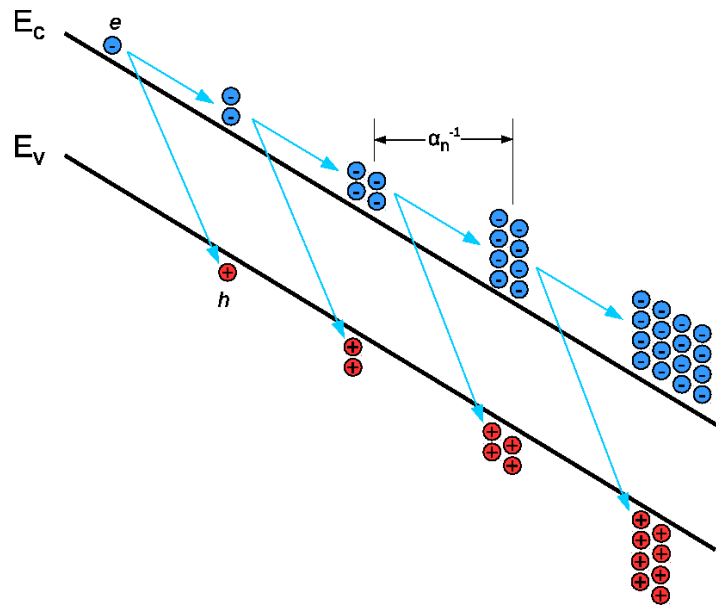
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200-300 kV/cm,

127 different kind of dopants. Since the electric field is high, usually above
128 carriers gain enough energy while travelling through this region to transfer it to elec-
129 trons through scattering, which can further ionize silicon atoms with electrons released

transfer it to elec-
electrons released

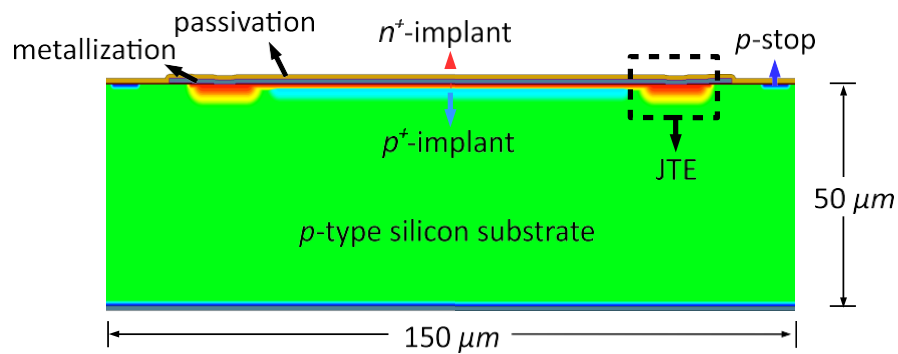
130 to the conduction band and holes to the valence band, creating new $e^- - h$ pairs (Sze,
131 2007), which can further create $e^- - h$ pairs as well, resulting in a cascade effect. As
132 an example, figure 1(a) shows the electron-induced impact ionization process. After
133 traveling a distance of α_n^{-1} on average, the electron undergoes a collision and a new
134 $e^- - h$ pair is generated. $\alpha_{n,p}$ is the impact-ionization coefficient for electrons or holes.
135 Since the impact-ionization coefficient of electrons is ~ 3 times higher than the one
136 of holes, the electron-induced impact ionization is the dominant process in LGAD
137 sensors (Maes, 1990).

138



a)

139



JTE: Junction-Termination-Extension

b)

Fig. 1. (a) Conceptual sketch of electron-induced impact ionization. After traveling a distance of α_n^{-1} on average, the electron undergoes a collision with new electron-hole pairs generated by its excess energies. (b) Cross section of the investigated LGAD sensors.

140

2. Detector description

141

142 LGAD microstrip sensors fabricated by Fondazione Bruno Kei
 143 were have been wire-bonded to single photon-counting and charge-integrat
 144 tronics developed at the Paul Scherrer Institut (PSI, Switzerland) in order to char-
 145 acterize their performance for soft X-ray detection. The LGADs have originally been
 146 developed for tracking charged particle with tens of pico-second resolution at the
 147 Large Hadron Collider (LHC), while the frontend electronics is optimized for hard
 148 X-ray detection using sensors with different geometry and opposite polarity, there-
 149 fore this work represents a proof of concept rather than a final development for the
 150 detection of soft X-rays using hybrid detectors.

151 2.1. The microstrip LGAD sensors

152 The investigated LGAD sensors are segmented into strips with a pitch of $150 \mu\text{m}$
 153 and a length of 5 mm . The thickness of the p -type float zone silicon substrate with a
 154 resistivity of $\geq 5 \text{ k}\Omega \cdot \text{cm}$ is $50 \mu\text{m}$.

155 The LGADs under investigation are n^+ -in- p sensors with the n^+ -side segmented
 156 (Paternoster, 2017). The charge multiplication layer is underneath the n^+ -implant,
 157 made by a layer of shallow p^+ -implant, either Boron or Gallium, whose distribution
 158 extends to a few μm below the n^+ layer. The cross section of a single strip is shown
 159 in figure 1(b). A Junction-Termination-Extension (JTE) has been implemented for
 160 each strip using deep phosphorous implantation embedding the multiplication layer
 161 (Temple, 1997; Fernandez-Martinez, 2016). The design of JTE ensures that no charge
 162 multiplication occurs when the $e - h$ pairs generated by charged particles or photons
 163 are absorbed in the gap region between two strips, thus the charge multiplication
 164 region of each strip is well-defined. The JTE limits the amplification region to the
 165 volume below the implant and practically defines a fill factor for the detection of the

166 amplified signal. A p -stop has been implemented in order to prevent a short between
167 strips due to the presence of oxide charges after fabrication and X-ray irradiation,
168 which induces an electron-accumulation layer below the SiO_2 layer.

169 The bulk capacitance of each strip is 1.63 pF from a calculation considering the
170 geometry the LGAD sensor, the interstrip capacitance to the first neighbor is 0.42 pF
171 and 0.05 pF to the second neighbor, with a total capacitive load of 2.57 pF at the input
172 of the frontend electronics. This value is higher compared to the 1.52 pF capacitance
173 measured for the planar silicon microstrip sensors (50 μm pitch, 320 μm thick, 8 mm
174 long) for which the readout electronics used in these experiments were designed (Moz-
175 zanica, 2009). Moreover, the settings of the frontend electronics have been optimized
176 for hole collection, while in the case of the LGADs under investigation the signal is
177 negative.

178 The LGAD sensors were manufactured and handled on top of a 570 μm thick, low
179 resistivity Czochralski wafer, which would absorb all the radiation if irradiated from
180 the backplane. For this reason, all the tests using X-rays have been performed by irra-
181 diating the sensor from the strip implant side. The nominal breakdown voltage is found
182 to be ≥ 300 V from the current-voltage (I-V) tests, thus all the X-ray measurements
183 have been done below 300 V.

184 Two LGAD microstrip sensors with different implantations and doses for the gain
185 layer have been investigated in this study: One with Boron, the other with Gallium.
186 The dose for Boron implantation is about 6% lower than Gallium. Sensors with iden-
187 tical layout as the LGADs but without multiplication layer have also been tested in
188 order to compare the performance of sensors with and without charge multiplication.

189 *2.2. The Mythen-II single photon counting readout*

190 The LGAD strip sensor with Boron implantation using a lower dose (wafer-1)
 191 has been wire-bonded to the Mythen-II photon-counting readout chip, which was
 192 developed for time-resolved powder diffraction experiments at synchrotron radiation
 193 sources. The Mythen-II chip consists of 128 channels operating in parallel (Mozzan-
 194 ica, 2009). Each channel has a charge-sensitive preamplifier that is AC coupled to two
 195 shapers followed by a comparator and a 24 bit counter. Only the signals exceeding an
 196 externally adjustable threshold are counted and therefore the detector is noise-free for
 197 energies above about ten times the electronic noise.

198 The Mythen-II readout chip is operated in electron collection mode for the LGAD
 199 sensors while still using the same standard settings which are normally used for hole
 200 collection (Bergamaschi, 2010). The ENC expected for the input capacitance of 2.57 pF
 201 corresponding to the LGAD microstrip is about $300 e^-$ RMS (~ 1100 eV), which would
 202 result in a minimal detectable energy of almost 11 keV compared to ~ 8.5 keV for stan-
 203 dard planar sensors with these settings (~ 5 keV with low noise settin
 204 2010)).

205 *2.3. The Gotthard-1.7 charge-integrating readout chip*

206 A different LGAD strip sensor with Gallium implantation using a higher dose (wafer-
 207 14) and therefore a higher gain has been wire-bonded to Gotthard-1.7, a charge-
 208 integrating prototype readout chip developed for X-ray Free-Electron Lasers (Zhang,
 209 2017; Zhang, 2018). It features a pre-chargeable dynamic gain switching pre-amplifier
 210 (PRE) with three gains with increasing feedback capacitance as described in (Moz-
 211 zanica, 2012) and a fully differential correlated-double-sampling (CDS) stage shared
 212 by four readout channels. The PRE output of each channel is connected to a Signal-
 213 and-Reset Sampling Stage (SRSS) which consists of two sets of analogue storage cells.

214 In each set of analogue storage cells, one storage cell is used to record the output of
215 the PRE immediately after reset while the other stores the additional signal induced
216 by the incoming photons. The outputs of the SSRS are multiplexed in group of four
217 channels to one fully differential CDS stage. Signals on the two analogue storage cells
218 are subtracted and amplified by the differential CDS stage so that the CDS differential
219 output is proportional to the integrated charge from the X-ray. Two sets of analogue
220 storage cells are implemented in each channel for dead-time free operation: while one
221 set is connecting to the PRE and storing the output signal from the PRE, the other
222 is disconnected from the PRE and being sampled and processed by the CDS.

223 3. Measurements

224 3.1. Leakage current

225 The leakage current of the LGAD microstrips at different bias voltages has been
226 measured using the Gotthard-1.7 readout chip. Figure 2(a) shows a linear dependence
227 as a function of the integration time for the detector output in absence of radiation at
228 different bias voltages. The leakage current can be estimated by fitting the data with
229 a straight line and converting the angular coefficient into a current using the energy
230 conversion gain g as explained in section 3.2.

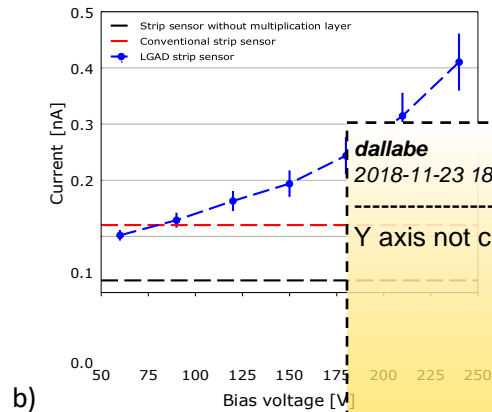
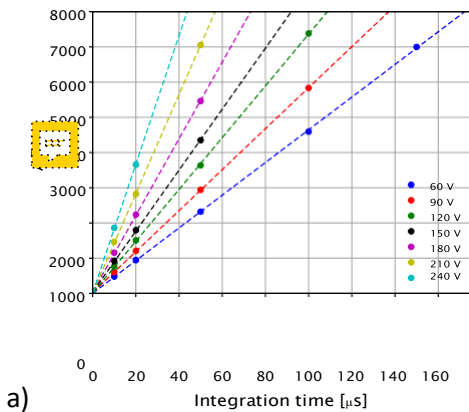
231 The averaged value of the extracted leakage currents for each individual strips as
232 function of bias voltage is shown in figure 2(b). In the voltage range from 60 V to 240 V,
233 the leakage current increases from 0.10 ± 0.01 nA to 0.41 ± 0.04 nA due to the increase
234 of the multiplication factor. For silicon strip sensors without multiplication layer and
235 conventional strip sensors, the leakage currents are 0.02 nA and 0.12 nA respectively,
236 with little dependence on the bias voltage after the sensor is fully depleted. The
237 difference between these sensors is attributed to the different layout design and sensor
238 thickness, as well as the quality of silicon substrate and oxide (e.g. carrier life times

239 and surface recombination velocities). The LGAD sensor shows higher leakage current
 240 than both, but it is still in a range which can be handled by the readout chip.

241 A high leakage current of the sensor results in an increase of the shot noise and
 242 therefore a higher electronic noise. Moreover, for CI readout chips, a high leakage
 243 current also leads to a reduction of the dynamic range. The Gotthard-1.7 readout chip
 244 is optimized for hole collection and has only a limited linear range for the negative
 245 polarity (about half of the 14 bit output). A maximum integration time of $\leq 50 \mu\text{s}$ can
 246 be used at bias voltage of 240 V, compared to $\leq 175 \mu\text{s}$ at 60 V; however, in all cases
 247 it is much longer than the $25 \mu\text{s}$ (at 40 kHz frame rate) readout time of the chip i.e.
 248 the detector can be operated in dead-time free mode also using LGADs.

249

250



251 Fig. 2. (a) Dynamic range scan using sensor leakage current for a single strip. (b) Average leakage current over all strips measured using Gotthard-1.7 at different bias voltages compared with sensors without multiplication.

252 **3.2. Energy response**

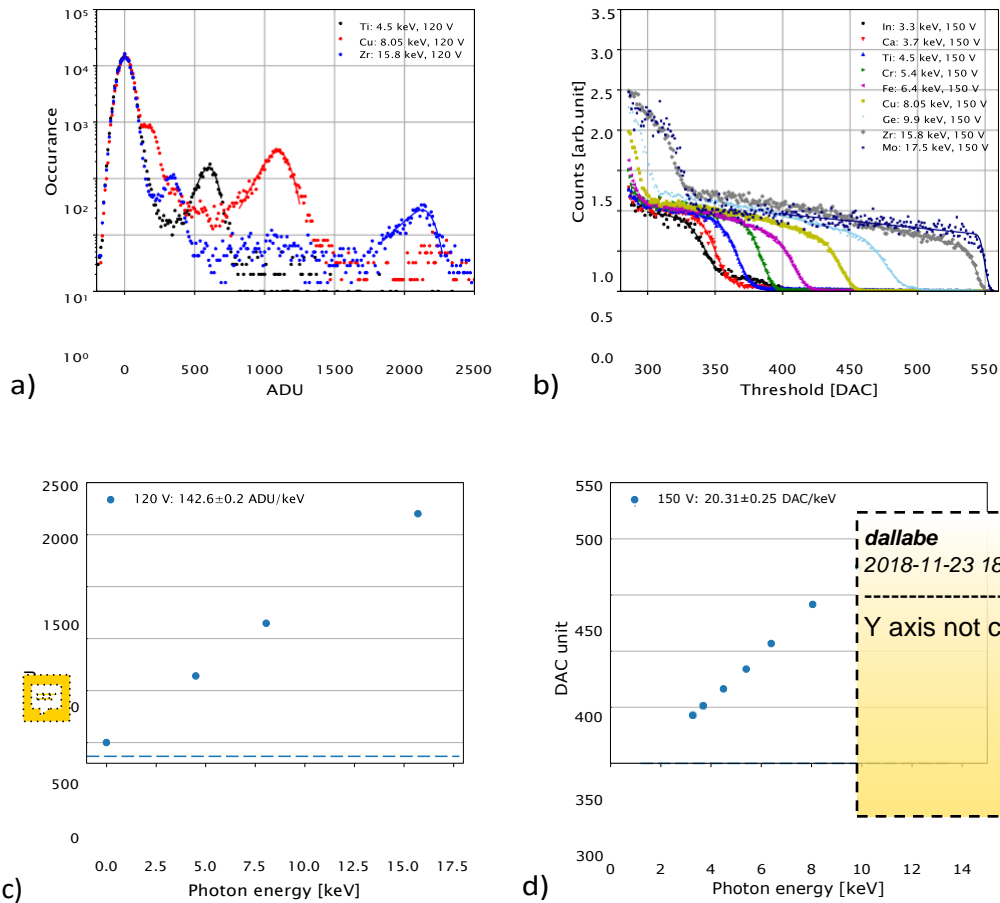
253 The LGAD strip sensors have been characterized using X-rays emitted by fluo-
 254 rescence targets of different elements excited using the beam generated by an X-ray
 255 tube (tungsten or chromium anode). The energy of the detected X-rays is quasi-

256 monochromatic with energies ranging between 3.3 keV (Indium L-edge) and 17.5 keV
257 (Molybdenum K-edge).

258 While the charge-integrating readout of Gotthard-1.7 allows the direct acquisition
259 of a full energy spectrum (pulse height distribution), the energy response of a single
260 photon-counting detector like Mythen-II is obtained by scanning the threshold of the
261 comparator. The resulting curve (S-curve) represents the integral of the spectrum and
262 contains equivalent information. Figure 3 show respectively (a) the spectra acquired
263 with Gotthard-1.7 at 120 V and (b) the S-curves acquired with Mythen-II at 150 V
264 for different X-ray energies, as well as the energy calibration of Gotthard-1.7 and
265 Mythen-II in (c) and (d).

266 In the case of Gotthard, the energy conversion gain g necessary to convert from ADC
267 unit into energy can be estimated by a linear fit of the peak position as a function of
268 the photon energy. For a photon counting detector, the energy conversion is extracted
269 by a linear fit between the position of the inflection point of the S-curves and the
270 photon energy, as described in detail in Bergamaschi (2010).

271



272

273

Fig. 3. Energy response of the LGAD microstrip sensors at different energies. a) Pulse height distributions acquired using the Gotthard 1.7 chip at 120 V bias voltage. b) S-curves acquired using Mythen-II at 150 V bias voltage. c) Energy calibration using Gotthard-1.7. d) Energy calibration using Mythen-II.

274 In both cases, for energies above 8.05 keV a shoulder is visible close to the noise
 275 level, which is due to X-rays absorbed in the region between the strips and which are
 276 not amplified. This signal can be used to estimate the multiplication factor i.e. the
 277 ratio between the conversion gain g with and without amplification and the fill factor
 278 i.e. the fraction of detected photons whose signal is amplified. Both the multiplication
 279 factor and the fill factor depend on the bias voltage applied to the LGADs.

280 *3.3. Multiplication factor*

281 The bias voltage applied to the LGAD sensors modifies the electric field in the
282 multiplication region and therefore affects the signal amplification. Figure 4 shows
283 (a) the pulse height distributions acquired using Gotthard-1.7 and (b) the S-curves

284 acquired using Mythen-II for X-ray fluorescence of 8.05 keV from copper target at
 285 different bias voltages. The shift of the peak in the spectra and of the inflection point
 286 in the S-curves show an increase of the conversion gain as a function of the applied bias
 287 voltage. The increase in the number of counts at higher bias voltages from Mythen-II,
 288 as shown in fig 4(b) is probably due to an extension of the amplification region with
 289 consequently higher fill factor (see section 3.5).

290 The multiplication factor, M , of the LGAD sensors is plotted in figure 5 and is
 291 estimated from the ratio between the conversion gain of LGAD sensors and planar
 292 sensors with the same layout but without multiplication layer. The multiplication
 293 factor ranges from 5 to 15 for the voltage range from 60 V to 240 V for the sensor
 294 with higher implantation dose and 4 to 6 for the sensor with lower implantation dose.
 295 The difference in multiplication factor of the two investigated sensors attributes to
 296 the different implantation doses and profiles for the gain layer.

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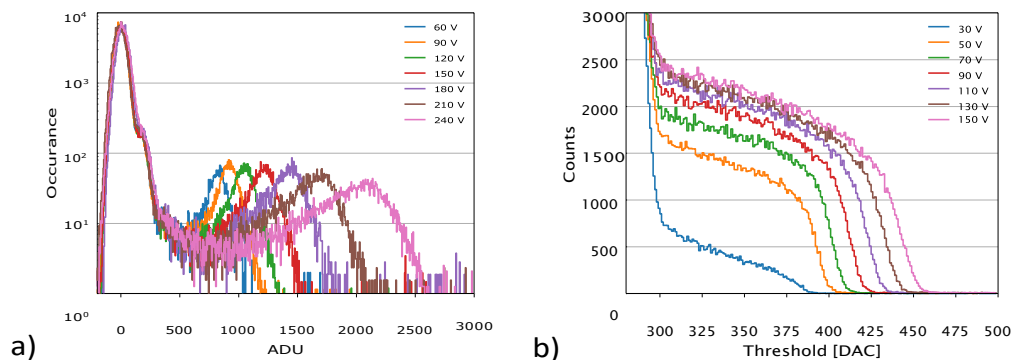
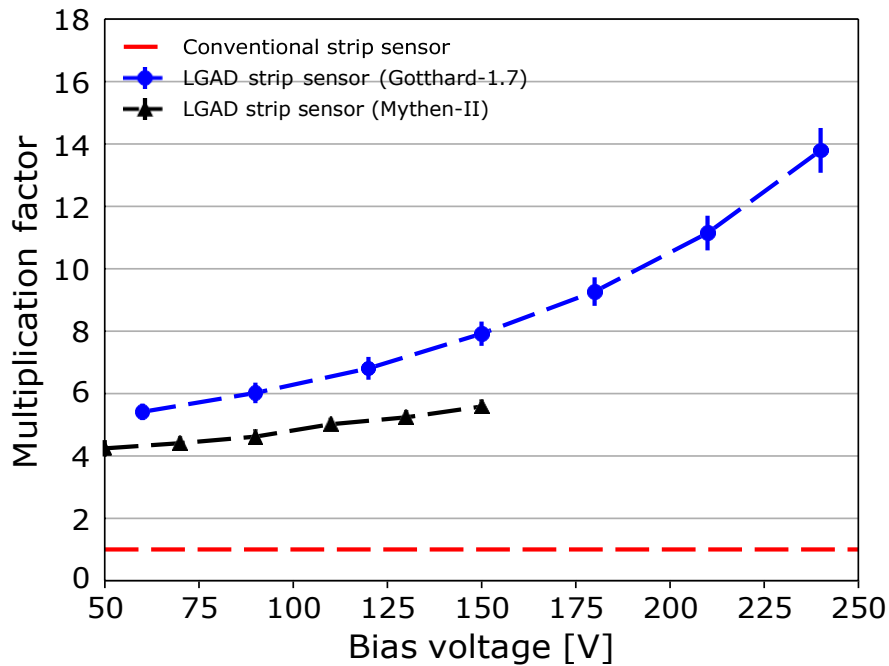


Fig. 4. Response to 8.05 keV copper fluorescence radiation at different bias voltages.

a) Pulse height distributions acquired using Gotthard-1.7 and b) S-curves acquired
 using Mythen-II.

299

300



301

Fig. 5. Average multiplication factor over all strips as function of the bias voltage for the two LGAD strip sensors investigated using Gotthard-1.7 and Mythen-II. The multiplication factors of the two sensors at the same bias voltage are different as they were fabricated using different implants and doses to form the multiplication layer.

302

303 3.4. Noise and energy resolution

304 For Gotthard, the noise has been estimated from the standard deviation of the
 305 spectrum in absence of illumination (equivalent to a Gaussian fit to the zero photon
 306 distribution), and converted into energy units by using the conversion gain g calcu-
 307 lated as in section 3.2). Figure 6(a) shows the noise as function of bias voltage. With
 308 increasing bias voltage, the noise in energy decreases since the noise remains con-
 309 stant in electron charge, which is independent of the signal amplification, while the
 310 conversion factor g increases.

311 In addition, the energy resolution has been calculated by fitting the width of the

³¹² single photon distributions and converting its standard deviation into energy using

313 *g.* The energy resolution vs. bias voltage of the LGAD sensor for 8.05 keV X-rays
 314 is shown in figure 6(a) as well. It is higher than the noise since it contains both the
 315 noise contributions and the variations in the multiplication factor due to the shot
 316 noise or to different absorption position. The energy resolution is $\sim 0.41 \pm 0.02$ keV
 317 below 180 V. Above 180 V, the pulse height still increases while the shot noise, due
 318 to large multiplication, starts to be dominant making the energy resolution at higher
 319 bias voltages worse. The best value of energy resolution at 8.05 keV happens at bias
 320 voltages of ≤ 180 V, corresponding to a multiplication factor of ~ 10 . Compared to the
 321 strip sensor without multiplication layer and the conventional strip sensor, the energy
 322 resolution has been improved by a factor of 5.5 and 2.7, respectively, in the LGAD
 323 sensor.

324 figure 6(b) shows the energy resolution depends also on the X-

325 shows that the energy resolution
 326 for low energy X-rays ($\leq 1-2$ keV)

326 rays i.e. can be improved before the shot noise being dominated for

327 by increasing the multiplication factor. At 240 V ($M \approx 13.8$), the ene

328 1 keV is ~ 0.21 keV, with a signal-to-noise ratio of about 5, which would

329 photon resolution. An optimized design of the LGAD sensor will improve the energy

330 resolution and further extend the minimal detectable energy, by using sensors with a

331 lower input capacitance compared to the one under test.

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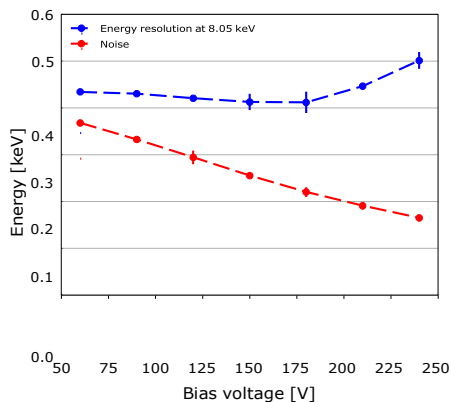
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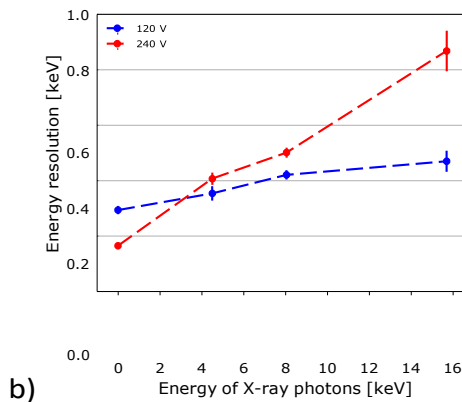
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could enable single

332



333



a)

b)

Fig. 6. (a) Average noise over all strip channels as well as energy resolution of 8.05 keV X-rays as function of bias voltage investigated using Gotthard. (b) Energy resolution as function of the photon energy at 120 V and 240 V.

334

335 In the case of a single photon-counting detector, the direct measurement of the noise
 336 is not possible, while the energy resolution can be estimated by the slope of the S-
 337 curve at the inflection point measured using monochromatic radiation (Bergamaschi,
 338 2010). Figure 7 shows the S-curve recorded at the PHOENIX beamline of the Swiss
 339 Light Source using 2.1 keV photons for one of the channels of Mythen-II. The strip
 340 are illuminated from the front side, i.e. where the gain layer is located.

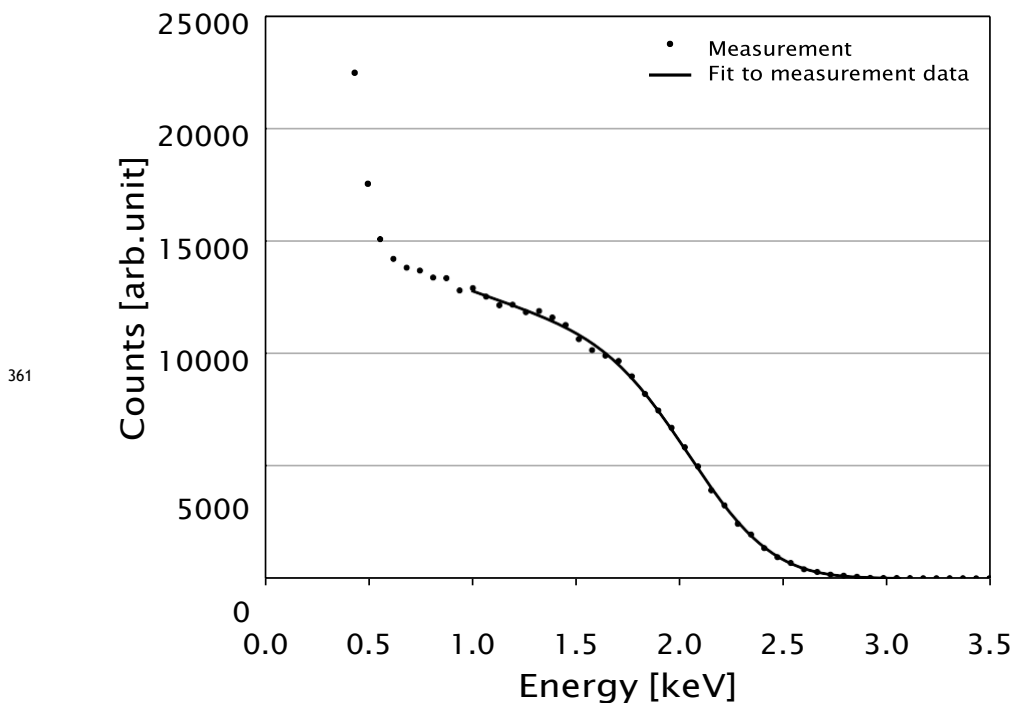
341 From the S-curve, a gain of 15.68 DAC/keV is obtained, which is $\sim 22.80\%$ lower
 342 than the gain of 20.31 DAC/keV extracted from the energy calibration shown in
 343 figure 3(d) at the same bias voltage of 150 V. This is partially due to the fact that
 344 the detector was operated in vacuum and therefore at a higher temperature compared
 345 to the measurements in air. Moreover, since the detector is illuminated from strip
 346 side, where the multiplication is located, and the attenuation length of the 2.1 keV
 347 photons in silicon is $1.74 \mu\text{m}$, most of the photons are absorbed in the gain layer.
 348 In this case, the electrons will travel a shorter distance in the gain layer, incurring
 349 in less impact-ionization events, with consequent reduced multiplication, while the

350 holes travelling through the gain layer have a lower impact-ionization coefficient. The
351 resulting multiplication coefficient is therefore lower compared to photons absorbed

352 in the sensor bulk underneath the gain layer. The different absorption depth within
 353 the gain layer will also increase the spread of the multiplication factor and therefore
 354 degrade the energy resolution.

355 The average energy resolution for all channels at 2.1 keV is 0.310 ± 0.024 keV RMS. It
 356 is reduced of more than a factor of 3 compared to the noise expected for a sensor of the
 357 same input capacitance based on hole collection which does not include the variations
 358 in the multiplication gain. We expect that this value can be further improved by
 359 effectively cooling the detector and by using back-illuminated fully depleted LGADs.

360



362 Fig. 7. S-curve of a single strip taken in direct beam of 2.1 keV at the PHOENIX
 beamline of SLS with a bias voltage of 150 V. The energy resolution estimated
 from the fit for this channel is 0.310 ± 0.003 keV RMS.

363 3.5. Fill factor

364 The JTE limits the multiplication region to the volume below the implant and

365 practically defines a fill factor for the detection of the amplified signal which also

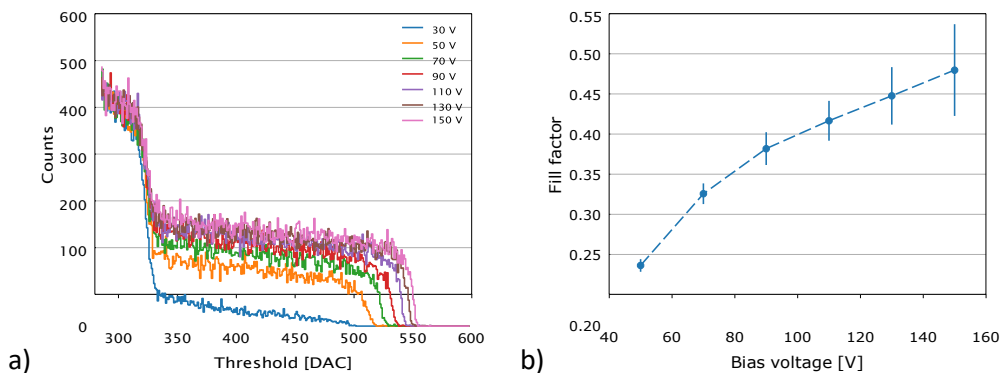
366 depends on the bias voltage. At low energies, the non-amplified X-rays cannot be
 367 detected and a low fill factor translates into a reduction of the quantum efficiency.

368 The S-curves acquired using 17.5 keV photons plotted in figure 8(a) show a second
 369 plateau at lower thresholds due to the X-rays absorbed in-between two strips, where
 370 no charge multiplication is present in the LGAD sensor. These photons are detected
 371 with a signal height like in the planar silicon sensor, while the photons absorbed in
 372 the multiplication region are amplified and create a larger signal.

373 The ratio of the number of counts of the amplified photons and the total number of
 374 photons gives the fill factor of the LGADs. Figure 8(b) shows the fill factor measured
 375 as a function of the bias voltage. At 50 V it is only 23.6 % at an more than doubles at
 376 150 V (48.0 %) showing that an increase of the electric field can partially improve it.

377

378



379

Fig. 8. (a) The S-curves from 17.5 keV X-ray fluorescence at different bias voltages using Mythen-II and (b) determined fill factors of the LGAD sensors at different bias voltages from the S-curves.

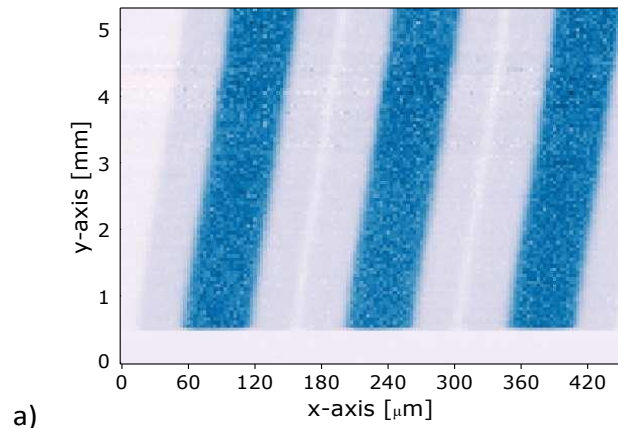
380 To further investigate the position dependence of the multiplication, the LGAD
 381 sensor read out using Gotthard was scanned in an X-ray beam of 20 keV focused
 382 to $\sim 3 \mu\text{m}$ by means of beryllium compound refractive lenses (Snigirev, 1998) at the
 383 European Synchrotron Radiation Facility. The sensor was biased to 120 V during

384 the measurement. The measured energy as function of beam position crossing three
385 strips is shown in figure 9(a) and their projection to the x -axis in figure 9(b). The

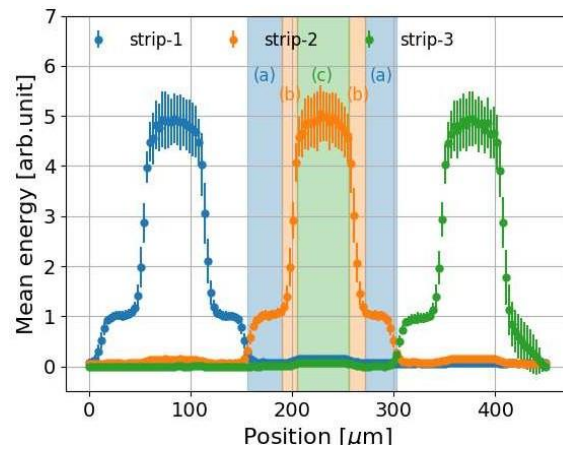
386 region with measured energy above 1 in the figure indicates the region with charge
387 multiplication. The fill factor, defined by the percentage of the area with measured
388 energy higher than 50 % of the maximum in the scan, is $\sim 40\%$, corresponding to
389 a width of $60\ \mu\text{m}$ and a gap of $90\ \mu\text{m}$ (without or with lower multiplication). Inside
390 the area with charge multiplication, the mean value of the measured energy varies at
391 different positions indicating a gain variation. From the measurement, it is shown that
392 the non-uniformity of the measured energy due to the gain variation is smaller than
393 the noise.

394 Figure 9(c) shows the spectrum of one investigated strip when X-rays illuminate
395 different regions: (a) The non-multiplication region ($M=1$), (b) the transition region
396 with and without multiplication, as well as (c) the multiplication region ($M=6.7$ at
397 120 V). The peak at zero ADU is caused by the noise of the system. In (a), up to three
398 single photon peaks, labeled as 1,2,3 ph ($M=1$), can be seen in the spectrum for the
399 photons without charge multiplication. The photon peaks are at 435 ADU, 870 ADU
400 and 1305 ADU for one, two and three photons, respectively. In (b), both single photons
401 with and without multiplication are visible. The single and double photon peaks at
402 435 ADU and 870 ADU remain visible, while a third peak at 2500 ADU arises due
403 to the signal multiplication of the single photons. In (c), only photons with charge
404 multiplication can be seen. Here, the single photon peak is located at 2935 ADU and
405 two photons create a signal of 5870 ADU. Note that the "single" photon peak with
406 charge multiplication in (b) shows slightly lower pulse height at 2500 ADU compared
407 to 2935 ADU for photons absorbed in (c) which has to be attributed to only partial
408 multiplication of the charges due to diffusion of electrons during drifting to the readout
409 electrode driven by the electric field inside the sensor.

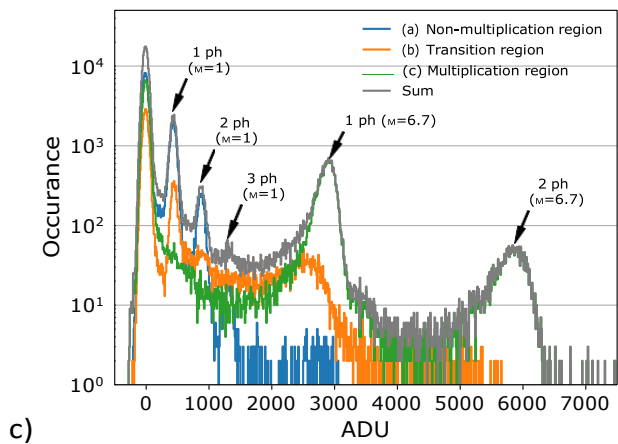
410



a)



b)



c)

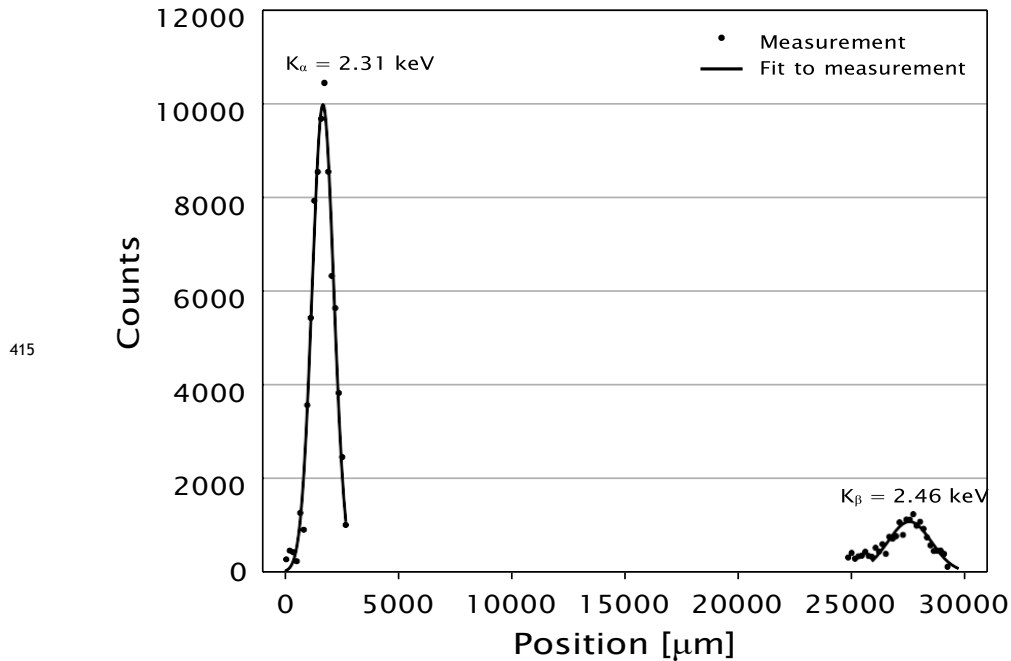
Fig. 9. a) Mean energy measured as a function of the position of the pencil beam on a region of three strips, b) a profile of the image and c) spectrum measured in the different regions. Labels in b) refer to the different regions shown in c).

411

410

413 4. Tender X-ray energy dispersive spectrometer measurements

414



415

416 Fig. 10. Fluorescence emission spectrum of Sulfur, taken with a von Hamos spectrom-
eter at the PHOENIX beamline of SLS.

417 As a proof of principle, the LGAD with the Mythen readout was tested in a von
418 Hamos spectrometer operating in the tender X-ray energy range (2-4 keV) installed
419 at the PHOENIX beamline of the Swiss Light Source (Huthwelker, 2018). The spec-
420 trometer normally uses the CI MÖNCH detector (Ramilli, 2017), which provides single
421 photon resolution at these energies. However, the detected flux is very low and a PC
422 readout, as normally used in the hard X-ray energy range, would be more appropriate
423 (Slatcheko, 2012).

424 Figure 10 shows a fluorescence emission spectrum of Sulfur recorded using an unfoc-
425 cused X-ray beam of 3 keV. The $K_{\alpha}=2.31 \text{ keV}$ and $K_{\beta}=2.46 \text{ keV}$ lines are located on

426 two separate sensors assembled on the same module. The fluorescence lines are well
427 detected even without threshold equalization, which is outstanding compared to the
428 minimum detectable energy of about 11 keV for the detector with planar silicon sen-
429 sors of the same geometry. For the standard sensor the detector limit is 5 keV thanks
430 to the smaller sensor capacitance and optimized settings.

431 The spectrum has been acquired in a single acquisition with an exposure time of
432 15 s. In order to acquire the same spectrum using MÖNCH, 15000 frames should
433 have been acquired and analyzed in order to extract the photons, requiring a high
434 performance data backend system.

435 Still, this measurement is only a proof of principle. The spectrometer would require
436 a spatial resolution of better than 50 μm in order to provide the expected 0.5 eV
437 energy resolution and separate e.g. the $K_{\alpha 1}$, $K_{\alpha 2}$ doublet using the focused beam.
438 This is clearly not yet achievable with the current sensors due to the large strip pitch
439 and low fill factor and will require further development of the LGAD technology.

440 5. Discussion

441 An LGAD strip sensor segmented on the n^+ -side has been investigated and results
442 demonstrate the possibility to extend the minimal detectable energy of X-rays for PC
443 and the single photon resolution for CI microstrip detectors down or below 2 keV.
444 These results have been obtained with sensors developed for ultrafast tracking of
445 charged particles, with a high input capacitance and readout electronics with rela-
446 tively high noise (ca. 300 e^- for Mythen-II and Gotthard-1.7, both optimized for hole
447 collection). Therefore we expect that this minimum energy can be improved down
448 to about 500 eV in order to include the L-edges of 3D transition metals by careful
449 optimization of the LGAD technology and matching of the readout electronics.

450 Moreover, for most X-ray applications, the segmentation of the sensors should be

451 reduced to at least 100 μm with a fill factor close to 100% in order to improve the
452 spatial resolution and the quantum efficiency. This can be obtained by optimizing
453 the design layout of the JTE, exploiting charge diffusion using back illuminated thick
454 silicon sensors or alternatively by developing inverse LGADs with the multiplication
455 layer on the rear side (Paternoster, 2017).

456 Pixel detectors require back illumination of the sensors, therefore LGADs without
457 substrate and with shallow backplane (≤ 200 nm implant) must be optimized in order
458 to obtain a high quantum efficiency below 1 keV.

459 This study represents only a proof of principle for using LGAD sensors for soft X-ray
460 detection. Despite the many technological challenges for improving the capacitance,
461 the leakage current, the segmentation and the quantum efficiency, we expect that
462 the LGAD technology could be a breakthrough for the development of soft X-ray
463 single photon counting detectors, which would be a game changer for several resonant
464 diffraction and spectromicroscopy applications.

465 Acknowledgements

466 The tender X-rays synchrotron radiation measurements have been carried out at
467 the PHOENIX beamline of the Swiss Light Sources. The pencil beam scan has been
468 performed at the BM05 beamline of the European Synchrotron Radiation Facility.

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Synopsis

Low Gain Avalanche Detectors have been characterized using X-rays. Preliminary tests show promising results towards the development of soft X-ray single photon counting detectors.
